

0039-9140(94)00260-6

# REVIEW

# HYPHENATED FLOW INJECTION SYSTEMS AND HIGH DISCRIMINATION INSTRUMENTS

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(Received 2 February 1994. Revised 2 September 1994. Accepted 2 September 1994)

Summary—An overview of the state-of-the-art in flow injection analysis (FIA) coupled to instruments capable of providing either multidetection and/or multi-information is reported. The versatility of FIA endows the hyphenated instruments with analytical capabilities which increase from simple sample introduction to more complex sample handling such as automatic dilution and calibration, solvent exchange, derivatization reactions and on-line separation processes, among others. Unexplored aspects of these powerful problem solvers are also discussed.

Unaffordable analytical problems have found proper solutions since the appearance of 'hyphenated techniques', a term coined by Hirschfield at the beginning of the last decade<sup>1</sup> to name the coupling of two or more powerful techniques or instruments to achieve a synergistic effect of their overall performance with respect to their separate use. Liquid,<sup>2,3</sup> gas<sup>4</sup> and supercritical fluid<sup>5</sup> chromatographic techniques interfaced with mass spectrometric or with atomic spectrometric instruments<sup>6</sup> are examples of the excellent performance of these complex systems, as is the mass spectrometry-mass spectrometry tandem.7 Most of the cases of hyphenated techniques entail powerful, large, expensive units, whose capabilities compensate for both high acquisition and maintenance costs.

Flow injection analysis  $(FIA)^{8-10}$  is a simple and inexpensive technique the versatility of which affords for developing steps of the analytical process of rather different complexity. The simplest use of FIA is as a way for introducing samples into a detector, which is far from demonstrating the capabilities of this technique. Nevertheless, this simple use enables the sampling frequency to be dramatically increased and reduce the sample and reagent consumption. More interesting is the use of FIA to implement on-line derivatization reactions,<sup>11</sup> separation processes<sup>12,13</sup> as well as a number of

sample handling modes to fit the initial sample conditions to the most suitable for single and multidetection<sup>14,15</sup> or implementation of flow-through (bio)chemical sensors,<sup>16-18</sup> among others.

Most of the detectors coupled to FI manifolds, either for sample introduction or for more complex sample handling, have been conventional instruments (e.g. molecular, atomic optical or electrochemical) capable of providing only two dimensional information. As happened with chromatographic techniques,<sup>19</sup> the first attempts to obtain three dimensional information in FIA were performed using either fast scan electrochemical<sup>20</sup> or diode array detectors,<sup>21</sup> thus enlarging the scope of application of FIA to more complex chemical systems. In a parallel but delayed development of hyphenated systems in chromatography, the coupling of FIA with high discrimination instruments pointed out the maturity of this dynamic technique. This last step in FIA started with the FIA-ICP-AES coupling. The capability of ICP-AES for multidetermination has been aided by FIA in different aspects since the earliest 1980's as listed in Table 141-103 and has been reviewed by different authors.<sup>22-24</sup> More recent and less numerous have been the arrangements of FI manifolds with instruments which enable three dimensional information and high

$ \begin{array}{c c c c c c c c c c c c c c c c c c c $		T	able 1. FIA-ICP	coupling			
CaSynthetic water, attern25-30090-320 $40-400$ Organ Ratern C, Cl, S)Water S, Er, Br in Ar)30300300 $0.139 \ gr/mlOrganC, Cl, S)WaterC, Cl, S, Cl, Br in Ar)303003000.139 \ gr/mlperformance studiestudies. OptimizationMetalC, Cl, S)WaterC, Cl, S, Cl, S, Cr, S, Strand30 \ \muld30 \ \muld0.139 \ gr/mlperformance studiesstudies. OptimizationMetalC, Cl, F, Mg)MetalC, F, Mg)90 \ \muld30 \ \muld90 \ \muld20 \ gr/mlPerformance studiesstudies. OptimizationMetalC, L, F, Mg)StateC, L, F, Mg)30 \ \muld30 \ \muld30 \ \muld30 \ \muld30 \ \muld30 \ \muld30 \ \muldMutalC, L, F, Mg)MetalC, L, F, Mg)30 \ \muld30 \ \muld<$	Analyte(s)	Sample(s)	Sample volume $(\mu l)$	Sampling frequency (hr <sup>-1</sup> )	Detection	Other aspects	Ref.
B     Values Cut, Pb, Zn.     Metric Secons annoles Cr, Br in Ar)     30     320 $ng mil$ (SF, SE in Ar)       Out, Pb, Zn.     Cut, Pb, Zn.     Secons annoles Cr, Br in Ar)     15-500     30, 90,     Performance studies So, 30, 80,     Performance studies So, 30, 80,       Metal     Non-metals (Br, Cu, Fe, Mg)     GF, Br in Ar)     So al, 30,     0, 30, 90,     20, 90,       Metal     Secons annoles     15-500     30, 40,     So againty     So againty       Metal     Secons annoles     15-500     30, 40,     Stopperimization       Cut, Fe, Mg)     Technological     90     43     Stopperimization       Cut, Fe, Mg)     Technological     90     45     0.02, 13     Runar Filer       So magnetic     114     114     Interference studies     Stoppin and on annoles     Stoppin annoles	Са	Synthetic, water,	25-300	90–320	40-400	-	41-43
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	В	Water	300	320	lm/gn		
	Organometallic Cd. Pb. Zn		50		0.139 µg/ml	Interface	44 45
Wetal Acerylactore     50 μl     Complex stability statutization (Cu, Fe, Mg)     Complex stability statutization (Cu, Mi, Zn)     Complex stability standard (Subility)     Complex stability statutization (Cu, Mg)     Complex stability standard (Subility)     Complex stability standard (Subility)       Kalman Filter     114     Nutletienents     8.4 ng/ml     Nutleterence studies       Nutletements     Synthetic     10     114     Nutleterence studies       Nutletements     Synthetic     100-500     45     0.02-1.3     Robotics       Nutletements     Synthetic     20-50     10.2-4.0     Nutleterence studies     Nutleterence studies       Sign     Systements     Synthetic     10-300     0.3-5.00     Interface studies	Non-metals (Br, C, Cl, S)	Gaseous samples (SF6, CF2C12, CF3Br in Ar)	15-500		50, 30, 80, 20 <i>pg</i>	performance studies	46
CurrentsesFine chementsFine chemicalsSurpractritical FI systeTace dementsTechnologicalSolSurpractritical FI systeCu. Fe, MgTechnologicalSolSolprocessing solutionSolSolSurpleticCa, MgSynthetic114Interference studiesCa, MgSynthetic114Interference studiesCa, MgSynthetic100-50045 $0.2-1.3$ RoutionSol45 $0.2-1.3$ RoboticsMutelementsSynthetic20-50 $10-340$ Reduced sampleSynthetic20-50 $10-340$ Reduced sampleSynthetic20-50 $10-340$ Reduced sampleSynthetic20-50 $10-340$ Reduced sampleSynthetic20-50 $10-340$ Reduced sampleSynthetic10-30060 $0.3-500$ Interference studiesSynthetic10-30060 $0.3-500$ Interference studiesSynthetic10 $0.3-800$ $100-900$ $0.9-100$ Si83% phosphoric $177$ $0.3-500$ Interference studiesSi81 <td>Metal</td> <td></td> <td>50 µl</td> <td></td> <td></td> <td>Complex stability studies. Optimization SFC-DAD-ICP system.</td> <td>47</td>	Metal		50 µl			Complex stability studies. Optimization SFC-DAD-ICP system.	47
Technological Standlogical   Rechnological 50 8.4 ng/ml   Focessing solution 50 8.4 ng/ml   Ca, Mg Synthetic 114   Ca, Mg Synthetic 114   Dadi (0 mg/ml Ti) 114 Interference studies   Wultielements Synthetic 100-500 45 0.02-1.3   Robotics 114 0.02-1.3 Robotics   Alloys 500 45 0.02-1.3 Robotics   Synthetic 10-300 60 0.3-500 10-340   Synthetic 10-300 60 0.3-500 Interference studies   Synthetic 20-50 10-340 Reduced sample   Synthetic 20-30 10-300 60 0.3-500   Synthetic 500 10-300 0.1-340 Reduced sample   Synthetic 500 177 00 10-340 Palury automization   Synthetic 500 177 00 0.3-500 Interference studies   Synthetic 500 177 00 0.3-500 Interference studies   Synthetic 500 177 00 0.10 0.10   Sint additon 00 0.2-500 Interference	complexes Trace elements (Cu, Fe, Mg)	Fine chemicals				Supercritical FI system FI slurry atomization	48
$ \begin{array}{ccccc} Ca, Mg & and 10 mg/mi Ti) & 114 & Interference studies. \\ Ca, Mg & Synthetic & 114 & Interference studies. \\ Wultielements & Synthetic & 100–500 & 45 & 0.02–1.3 & Robotics \\ Used & 500 & 45 & 0.02–1.3 & Robotics \\ Mloys & Mloys & 0.02–1.3 & Robotics \\ Mloys & Mloys & Mloys & 0.03–500 & 0.0-340 & Reduced sample \\ mg/mi & 0.03–500 & 0.0-3-500 & Interface studies \\ Synthetic & Synthetic & 0.0-300 & 60 & 0.3–500 & Interface studies \\ mg/mi & 0.03–500 & 0.0-3-500 & Interface studies \\ mg/mi & 0.0-300 & 60 & 0.3-500 & Interface studies \\ mg/mi & 0.3-500 & 10-300 & 0.0-3-60 & Interface studies \\ mg/mi & 0.3-500 & 10-300 & 0.0-3-60 & Interface studies \\ mg/mi & 0.3-500 & 10-300 & 0.0-3-60 & Interface studies \\ Synthetic & 500 & 0.3-500 & Interface studies \\ Si & 85% phosphoric & 177 & 0.110 & 0.110 & 0.110 \\ Cu & Bur filtrates & 150 & 110 & 0.110 & 0.110 \\ Rare-earth & Metal samples & 500 & 110 & 0.110 & 0.110 & 0.110 \\ Rare-earth & Metal samples & 500 & 110 & 0.110 & 0.110 & 0.110 & 0.110 \\ Multielements & Lubricating oils & 500 & 132 & 0.0110 & 0.110 & 0.110 & 0.110 & 0.110 & 0.00 & 0.0110 & 0.0110 & 0.0110 & 0.0110 & 0.0110 & 0.00$	Sc	Technological processing solution (containing ~ 30 mg/ml Fe	500		8.4 ng/ml		49
MultielementsSynthetic100–500 $0.5-6 ng/ml$ Kalman FilterUsed50045 $0.02-1.3$ RoboticsUbricating oils $0.02-1.3$ RoboticsBiological $20-50$ $10-340$ ReboticsBiological $20-50$ $10-340$ ReboticsSynthetic $0.02-1.3$ RoboticsSynthetic $0.02-1.3$ RoboticsSynthetic $0.02-1.3$ RoboticsSynthetic $0.02-1.3$ RoboticsSynthetic $0.02-50$ $10-340$ Reference oils $500$ $0.3-500$ Si85% phosphoric $177$ Si85% $100$ Si $100$ $100$ Si $100$ Si $100$ Si $100$ Si $11$	Ca, Mg	and 10 <i>mg/ml</i> Ti) Synthetic	114			Interference studies.	50
Maloys $\mu g/g$ On-line electrolytic disolAlloysBiological $20-50$ $\mu g/g$ On-line electrolytic disolBiological $20-50$ $10-340$ Reduced sampleSynthetic $\pi g/ml$ $10-300$ $60$ $0.3-500$ Interface studiesSynthetic $300$ $60$ $0.3-500$ Interface studiesSetReference oils $500$ $\pi g/ml$ Interface studiesSi $85\%$ phosphoric $177$ $222-88.8$ $900$ Si $85\%$ phosphoric $177$ $000$ $000$ Si $85\%$ phosphoric $177$ $0000$ $0000$ Si $85\%$ phosphoric $177$ $00000$ Si $85\%$ phosphoric $177$ $00000$ Si $85\%$ phosphoric $1100$ $00000$ Si $85\%$ phosphoric $1100$ $00000$ Si $85\%$ phosphoric $1100$ $000000$ Si $8000$ $1100$ $0000000$ Rate-carthMetal samples $00000000$ Cu, Ni, ZnAlloys $500$ $1100$ MultielementsLubricating oils $00000000$ Water $000000000000000000000000000000000000$	Multielements	Synthetic Used	100-500 500	45	0.5-6 ng/ml 0.02-1.3	Kalman Filter Robotics	43, 51 52
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(aqueous and relations) 10–300 60 0.3–500 Interface studies   Synthetic Synthetic 500 ngamic solutions) Interface studies   Synthetic Synthetic 500 0.3–500 Interface studies   Stepson Southetic 500 0.3–500 Interface studies   Stepson Stepson 500 0.3–500 Interface studies   Stepson Stepson 22.2–88.8 00 0.110   Si 85% phosphoric 177 0.110 0n-line dilution   Cu Burt filtrates 150 110 0n-line standard   Rare-earth Metal samples 00 110 0n-line standard   Cu, Ni, Zn Alloys 500 132 0n-line standard addition   Cu, Ni, Zn Plant digests 100 132 0n-line standard addition   Multielements Lubricating oils 100 132 0n-line standard addition   Water 60 500 500 500 0n-line standard addition		samples Svnthetic			lm/gn	reduced sample volume	54, 55
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Water 60 Standard salinity matchi	Multielements	Lubricating oils	100	132 80		On-line standard addition	69
		Water		90 90		Standard salinity matching	0/

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		73		74	31	C1 AF	2	77-78			62	80	2	81	87	70		83	84	L C	85	86		87-89	••	90, 91	92	93		continued
Time-based injection On-line standard	On-line standard addition (computer-guided). Time-based	injection addition (zone	sampling)	Amberlyst A-26,	mercaptoacetoxy-cellulose	Activated alumina	Activated aumima	Chelex 100,	Amberlite, Dowex	Amberlite XA-743	resin. Time-based	injection C honded silica	CI8 DOILDER SILLER MIP*-AES	Activated alumina	Anion-exchange	(AUL-X0 resur). On-line oxidatin to I,		Acidic alumina	Activated alumina	C <sub>18</sub> bonded silica.	Speciation by chromatography_MIP*-AFS	Chelex 100. In	parallel columns	Chelating resin,	basic alumina	Desolvation device	Chelating-cellulose	Chelating-cellulose	Al and Na removal	
				1 ng/ml		0.2 ng/ml	0.05 ng/ml	3 ng/ml					0.10 ng/mi	0.6 µg/ml		0.75, 31 no lml	111/211	2.8 ng/ml			0.15-0.2 pg	0.008 - 20	ng ml	0.009-2	lml gn	0.3–5.1 no/m/	0.0021 - 0.12	g/g4		
		001	071	9								č	30	45								30	2	12-20			20			
15	15	003	nnc	10 ml (250	eluent)	10-50 <i>m</i> /	10 <i>ml</i>	1000 (100	eluent)		250		1 <i>ml</i>	200		10 <i>ml</i>		2 <i>ml</i> (200 eluent)	200		10-50 ml	(250 eluent)		7.5 -80 ml		0.5 2.5 ml	35 ml			
Botanical SRM	Botanical SRM	-	Rocks KM	Refinerv	effluent water	Seawater	Human urine	Potable waters and	haemodialysis	fluids			Synthetic seawater	Steels				Natural waters, seawater, boiler-feed	water		River water		Synthetic	Waters		Serum	Alkali metal	salts	Aluminium alloys	
				Ŷ	nv	Mo	Cr(111)	14	đ		æ	2	Cu	۵.	•	I <sup>-</sup> , IO <sub>3</sub> <sup>-</sup>		$SO_4^{2-}$	Oxvanions	CAVAIIIN	Organotin	compounds	Multielements							
					Un-line separation	t inuid_solid	interfaces																							

## FIA and high discrimination results

	Ref	94	1 95 1	iplex) 96	26	86 86	66	100-105 tor)	106	201 107	108	601	110	111 88	111, 00	111, 00
	Other aspects	Donnan dialysis	preconcentration Indirect determination liq-lic extraction (La-alizari	complexone fluoride com Liq-liq extraction. Microporous PTFE	Liq-Liq extraction	(dithizone in UCl <sub>4</sub> ) Liq–liq extraction. Suction-cup sampling	Evaporation of inorganic C	Hydride generation (with and without microporous PTFE membrane/tubing separa	Hydride generation. Microporous PTFE separator	Hydride generation. Continuous flow system	Hydride generation	Hydride generation	Hydride generation	Acidic alumina		column
	Detection	pg/ml	30 ng/ml	50 ng/ml	0.1 ng/ml	0.4 ng/ml	5 mg /l	0.025–5.2 ng/ml	0.4 ng/ml	0.19 ng/ml	3.5, 7.0, 3.6 ng/ml	0.2, 0.2, 0.1	H5/8	1.4, 0.2	-	lm/gq
pen	Sampling frequency (hr <sup>-1</sup> )	2-8	36	25	25	20		120-200	150							
Table 1. contin	Sample volume $(\mu l)$	350-500 ml	200	500	3 ml	5 ml		40374	1000		750			2 ml (200 µl	1	eluent)
	Sample(s)	Salts solutions	Waters	Mg-Al alloys, Cu alloys	SRM water	SRM (biological) Water	(containing 500 mg/l of carbonate carbon)	Synthetic, SRM, glycerine, geological, NaCl and AlCl, Sinole-rrystal	gallium arsenide (non-, Zn- and Si-dop Al) and poly(ethylene- terephthalate)	Copper metal, waste water	Surface waters	Ure rock	SRM (steel, coal fly ash, urban particulate, river and seawaters)	Reference		walers Waste waters
	Analyte(s)	Metals	ц Ц	æ	Cu	P	Organic C	As Ge		Sb(III), Sb(V)	As, Sb, Se	AS, 20, <b>B</b> I	Multielements	Cr(III), Cr(IV)		Sb(III). Sb(V)
	FIA contribution		On-line separation process (II). Liquid-liquid interfaces				On-line separation process (III). Gas-liquid	interfaces						Speciation		
	Technique															

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\*Microwave plasma torch AES.

Ion lens tuning 117 strategies	Inductory J Ion lens tuning 117 strategies 118 Avoidance interface 118 clooging 119 Simplex optimization 120	Ion lens tuning strategies Avoidance interface clooging Simplex optimization Solid content: 5–10% [21 Comparison with leser-blation	Ion lens tuning strategies Avoidance interface clooging 119 Simplex optimization Solid content: 5–10% Solid content: 5–10% Comparison with laser-ablation Ion lens tuning strategies	Inductory 1 Ion lens tuning 117 strategies 118 clooging 119 Simplex optimization 120 Solid content: 5-10% 121 laser-ablation 122 laser-ablation 123 strategies 124	Intervence interface to the strategies avoidance interface 117 strategies 118 clooging 119 clooging 119 clooging 119 clooging 119 clooging 119 clooging 120 comparison with 120 laser-ablation 122 laser-ablation 122 laser-ablation 123 strategies 123 strategies 124 Off-line ion-exchange 125 and icotron dilution 125 and ico	Ion lens tuning117Ion lens tuning117strategies118clooging119clooging119Simplex optimization120Solid content: 5–10%121Comparison with122laser-ablation123laser-ablation123strategies123off-line ion-exchange125and isotope dilution126	Ion lens tuning117Ion lens tuning117strategies118clooging119clooging119Simplex optimization120Solid content: 5-10%121Comparison with122laser-ablation123faster-ablation123fon lens tuning123strategies124Off-line ion-exchange125and isotope dilution126	Ion lens tuning strategies117Ion lens tuning strategies117Simplex optimization128Comparison with laser-ablation121Ion lens tuning strategies123Off-line ion-exchange125and isotope dilution126Feeding experiments128	Ion lens tuning 117   Ion lens tuning 117   strategies 118   clooging 119   Simplex optimization 120   Solid content: 5–10% 121   Comparison with 122   laser-ablation 123   laser-ablation 123   laser-ablation 123   on lens tuning 123   strategies 124   Off-line ion-exchange 125   and isotope dilution 126   Freding experiments 128   Optimization study prior to 129, 130   HPI C-ICP_MS conting 129, 130	Ion lens tuning117Ion lens tuning117strategies118clooging119Simplex optimization120Solid content: 5-10%121Comparison with122laser-ablation123laser-ablation123lon lens tuning123strategies124Off-line ion-exchange125and isotope dilution126Teeding experiments129Optimization study prior to129, 130HDLC-ICP-MS coupling131Minimized matrix131	Ion lens tuning strategies117Ion lens tuning strategies117Simplex optimization129Simplex optimization120Solid content: 5-10%121Comparison with laser-ablation121Ion lens tuning strategies123Strategies124Off-line ion-exchange125and isotope dilution126Feeding experiments128Optimization study prior to deposition129, 130HPLC-ICP-MS coupling Minimized matrix132-136	Ion lens tuning   117     strategies   118     clooging   119     Simplex optimization   120     Solid content: 5–10%   121     Comparison with   122     laser-ablation   123     strategies   124     Off-line ion-exchange   125     and isotope dilution   126     Feeding experiments   128     Off-line ion-exchange   126     Ion lens tuning   123     strategies   124     Off-line ion-exchange   125     and isotope dilution   126     Preceding experiments   128     Optimization study prior to   129, 130     Minimized matrix   129, 130     Minimized matrix   131     deposition   132-136     Interfaces   137     introduction volatile   137     fintroduction volatile   137
	2.7 ng/ml &	2.7 ng/ml A Si sub-ng/g 0.2 ng/g Si	2.7 ng/ml A Si Sub-ng/g 0.2 ng/g St	2.7 ng/ml A Si sub-ng/g 0.2 ng/g	2.7 ng/ml A 2.7 ng/ml Si sub-ng/g Si 0.2 ng/g Si 0.2 ng/g O 5-14 pg O	2.7 ng/ml A 2.7 ng/ml Si Sub-ng/g Si 0.2 ng/g Si 0.2 ng/g Si 5-14 pg 0 1 ng/ml a	2.7 ng/ml A 2.7 ng/m sub-ng/g Si 0.2 ng/g Si 5-14 pg a 1 ng/ml a 0.2 ng/ml	2.7 ng/ml A 2.7 ng/ml Si sub-ng/g Si 0.2 ng/g Si 5-14 pg 0 1 ng/ml a 0.2 ng/ml F	2.7 ng/ml A 2.7 ng/ml Si sub-ng/g Si 0.2 ng/g Si 0.2 ng/ml a 0.2 ng/ml F F	2.7 ng/ml A Si sub-ng/g Si 0.2 ng/g Sc 5-14 pg a 1 ng/ml a 0.2 ng/ml F 0.2 ng/ml F	2.7 ng/ml A 2.7 ng/ml Si sub-ng/g Si 0.2 ng/g Si 1 ng/ml a 1 ng/ml A 0.2 ng/ml F 0.2 ng/ml F 0.2 ng/ml HPI	2.7 ng/ml A 2.7 ng/ml Si sub-ng/g Si 0.2 ng/g O 1 ng/ml a 0.2 ng/ml F 0.2 ng/ml F 0.2 ng/ml in 0.52-2.0 ng/ml ii
		30	30	30	30	30	30	30	90	90 90	90 90	90
	100	100 250	100 250 500	100 250 500	100 250 500 250, 500	100 250 500 250, 500 200	100 250 500 250, 500 <1000	100 250 500 250, 500 < 1000	100 250 500 250, 500 < 1000 < 1000	100 250 500 250, 500 <1000 <10-25 500	100 250 500 250, 500 200 < 1000 < 1000 25, 100	100 250 500 200 < 1000 < 1000 200 25, 100 50
	SRM (biological) Biological Human faeces	SRM (biological) Biological Human facces Peridotite Aluminium	SRM (biological) Biological Human facces Peridotite Aluminium Synthetic seawater	SRM (biological) Biological Human faeces Peridotite Aluminium Synthetic seawater Powdered, blood	SRM (biological) Biological Human facces Peridotite Aluminium Synthetic seawater Powdered, blood plasma Natural water, sediments	SRM (biological) Biological Human facces Peridotite Aluminium Synthetic seawater Powdered, blood plasma Natural water, sediments Natural water, sediments Natural actor	SRM (biological) Biological Human facces Peridotite Aluminium Synthetic seawater Powdered, blood plasma Natural water, sediments Natural water, sediments Nickel-base Blood plasma, serum	SRM (biological) Biological Human faeces Peridotite Aluminium Synthetic seawater Powdered, blood plasma Netural water, sediments Nickel-base alloys Blood plasma, serum Human faeces	SRM (biological) Biological Human facces Peridotite Aluminium Synthetic seawater Powdered, blood plasma Natural water, sediments Nickel-base alloys Blood plasma, serum Human facces Synthetic	SRM (biological) Biological Human facces Peridotite Aluminium Synthetic seawater Powdered, blood plasma Natural water, sediments Netural water, sediments Netural water, sediments Netural water, sediments Netural water, sediments Netural water, sediments Netural water, sediments Netural water, sediments Netural water, serum Human facces Synthetic SRM (rock)	SRM (biological) Biological Human faeces Peridotite Aluminium Synthetic seawater Powdered, blood plasma Netural water, sediments Blood plasma, serum Human faeces Synthetic SRM (rock) Organometallic compounds, sediments, allovs	SRM (biological) Biological Human faeces Peridotite Aluminium Synthetic seawater Powdered, blood plasma Netural water, sediments Nickel-base alloys Blood plasma, serum Human faeces Synthetic Synthetic SrRM (rock) Organometallic compounds, sediments, alloys Trace metals
(	Organomercury Thimerosal Trimethylgallium etherate	Organomercury Thimerosal Trimethylgallium etherate Pt-group metals U, Th	Organomercury Thimerosal Trimethylgallium etherate U, Th Ba, In	Organomercury Thimerosal Trimethylgallium etherate Pt-group metals U, Th Ba, In Pb, Zn	Organomercury Thimerosal Trimethylgallium etherate U, Th Ba, In Pb, Zn Re, Pb, Ir	Organomercury Thimerosal Trimethylgallium etherate Pt-group metals U, Th Ba, In Pb, Zn Re, Pb, Ir Tl, Pb, Bi	Organomercury Thimerosal Trimethylgallium etherate Pt-group metals U, Th Ba, In Pb, Zn Re, Pb, Ir Tl, Pb, Bi Au, Zn, Cu	Organomercury Thimerosal Trimethylgallium etherate Pt-group metals U, Th Ba, In Pb, Zn Re, Pb, Ir Tl, Pb, Bi Au, Zn, Cu Zn-64/Zn-67	Organomercury Thimerosal Trimethylgallium etherate Pt-group metals U, Th Ba, In Pb, Zn Re, Pb, Ir T1, Pb, Bi Au, Zn. Cu Zn-64/Zn-67 ratio Multielement	Organomercury Thimerosal Trimethylgallium etherate Pt-group metals U, Th Ba, In Pb, Zn Re, Pb, Ir Tl, Pb, Bi Au, Zn, Cu Zn-64/Zn-67 ratio Multielement	Organomercury Thimerosal Trimethylgallium etherate Dt-group metals U, Th Ba, In Pb, Zn Re, Pb, Ir Tl, Pb, Bi Au, Zn, Cu Zn-64/Zn-67 ratio Multielement	Organomercury Thimerosal Trimethylgallium etherate Pt-group metals U, Th Ba, In Pb, Zn Re, Pb, Ir Tl, Pb, Bi Au, Zn, Cu Zn-64/Zn-67 multielement

	Ref.	138, 139	140		141	142		143	144	145	146 147		148 149		131 031	101,001
	Other aspects	Isotopic dilution	On-line standard	addition method	On-line standard addition method	Continuous sample	standard mixing, high solid content	Dowex 1-x-8 (ReO <sup>4</sup> ) Isotonic dilution	Dowex 50 W-X8 (matrix retention)	On-line proconcentration matrix removal	In-parallel columns On-line anodic	stripping voltammetry	Hydride generation Hydride generation	Isotopic dilution PTFE tubing	separator	Hydride generation- vapour generation
	Detection					0   0 U	0,0	0.27 pg/ml	0.1 ng/ml		2 ng/ml 27 ng/ml	545 pg/ml	(Cd) 1.8 ng/ml 40 ng/ml	5		4-6 pg/l
ed	Sampling frequency (hr <sup>-1</sup> )	040	01 01	10	10-15				12							20
Table 2. continu	Sample volume ( ul )	3101	C/01	000	200	QOC	007	10–50 <i>ml</i>	800	10 <i>m</i> l (0.2 <i>m</i> l eluent)	50 ml	1000	40			500
	Samnle(s)	(a)arduna	NIS SKM 983 NIS SRM 991	Undiluted urine	Highly conc.	H, PO <sub>4</sub> and NH <sub>4</sub> NO <sub>3</sub>	High purity Ni	Seawater	Airborne	particulate Concentrated brines (30%)	SRM (seawater) Hair, SRM	SKM (urine)	SRM (rock)	SKMI, galelle		Seawater
	Ambitale	Allalyte(s)	Pb (isotopes)	Multielement				Re	Ł	Trace metals	Multielement	Cu, Cd	Ξ,	q		Hydride-forming elements Ho
	FIA	contribution	Sample handling	)				On-line	separation process (I)	Liquid-solid interfaces			On-line	process (III).	Cas-Induid interfaces	
		Technique														

			Table 3. Other Fl	IA/high discrimin	ation detector couplin	Sa		
Technique	FIA	A najvte(s)	Samula(c)	Sample	Sampling frequency (br -1)	Detection	Other senants	Def
Iccurrence		Unary uc (s)	(c)ridiupo		iteducine) (vii )	11111	Outer aspects	VCI.
FTIR	Sample introduction	Phenyl isocianate	Synthetic	25	60	4 μg/ml		152
		o-Xylene	Xylol	200	20	0.02% v/v	Comparison flow cells	153
		Ibuprafen	Pharmaceuticals	320	20	80 μg/ml	Partial dissolution in Cl <sub>4</sub> C	154
		Carbaryl	Pesticide formulations	300	53	1.6 μg/ml	Flowing or stop-flow modes	155
		Allyldiisopropylamine oxide	Synthetic		60		Carrier: supercritical CO,	156
		Aliphatic esters	Synthetic	130	25	14 mM	Comparison flowing and stop-flow modes	157
		Choline	Pharmaccutical		60	0.02 fg/ml	$\mu$ -CIRCLE cell	158
		compounds	preparations					
		Xylene	Commercial	200	20	0.02% v/v	$\mu$ -SPEAC cell	159
	Sampling handling	Benzene	Gasoline	300	18	0.02% n/n	On-line standard addition	160
	0	tert-Butyl ether	Unleaded	320	45	0.035% v/v	First order derivative	191
	-		gasolines					
WS	Sample introduction	I ributyltin	Sediment, SRM	200	50	0.2 µg Sn/g	Ion spray MS-MS Selected reaction monitoring	162
		Acetic acid, acetoin, 2,3-	Fermentation broth	250	15		MS-MS gas diffusion	163, 164
		outanedioi, ethanol, CO,, O,						
		Toxins	Plankton			2 µg/ml	Ion spray MS/MS	165
		$\beta$ -Blocking drugs	Pharmaceuticals			0.2 ng	Selected for monitoring Study prior to	166
						•	LC-MS coupling	
	Sample handling	Acetaminophen, olutathione cysteine	Synthetic	100			On-line electrochemical and chemical reactions	167
	On-line separation	As, Se, Sb, Sn	Synthetic	100		$0.1-1 \ \mu g/ml$	Hydride generation	168, 169
VECV	process	Chloroform	Synthetic	ſ	001	$\int \mu g/m l$	Gas diffusion	169
MECA	introduction	ouganophosphorous compounds, insectioides	ayınıncın	ч	2	7 XH 0C-C.0	between injections	1/0,1/1
		Sulphide, sulphide,	Synthetic	5	20	l ng S	No cavity cooling	172
	On-line separation	Arsenic	SRM (vegetal)	120	100	80 ng/ml	Hydride generation	173
NMR	process Sample introduction	Toluene	Acetonitrile	50		130 µg/ml	Evaluation flow-cell	174
Flame IRES	Sample introduction	Total inorganic carbon, saccharides	Tap water	25, 250	60		Design purge-cell FI and continuous modes	175

## FIA and high discrimination results

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discrimination capabilities like MS (by direct coupling or through an ICP source), FTIR and NMR, among the most important, which have also been reviewed,<sup>35-40</sup> and whose most significant features are listed in Tables 2<sup>114-151</sup> and 3.<sup>152-175</sup>

Figure 1 shows the dissimilar use of flow injection analysis-high discrimination instrument (FIA-HDI) couplings. For this reason the aim of this work is to give to the analytical community, but particularly FIA users, an overview of the present situation of these hyphenated techniques, emphasizing the advantages involved in them, criticizing their negative aspects and showing the unexplored availabilities of one of the most promising uses of FIA.

#### INTERFACES

The connection between a flow injection system and a high resolution detector has a decisive influence on the performance of the hyphenated system, as analytical quality parameters such as reproducibility, accuracy, sensitivity and selectivity are highly dependent on how this coupling is accomplished. The complexity of the interface is very different depending on whether the measurement is performed in solution, plasma or vacuum.

Inexpensive flow-cells (either conventional or demountable micro-flow cells) with KBr windows and different thickness spacers (0.015–0.22 mm, 0.15–9  $\mu$ l cell volume) are used in FIA–FTIR coupling when organic solvent



Fig. 1. Tridimensional plot of the main contributions of flow injection analysis coupled to high discrimination detectors. (Sp) Speciation; (g-l) gas-liquid; (l-l) liquid-liquid; (l-s) liquid-solid; (S.P.P.) on-line separation processes; (S.H.) sample handling and (S.I.) sample introduction.

carriers are involved.<sup>143–145,159–161</sup> The use of thick spacers yields a higher contribution to the blank measurement from the carrier solvent, so poorer detection limits are obtained. More sophisticated cells are used with uncommon solvents. A 25  $\mu$ l-micro-Circle cell equipped with a zinc selenide crystal (0.318 cm diameter) has been used for aqueous samples in FIA–FTIR;<sup>157,158</sup> and a high pressure flow cell (2  $\mu$ l, 1 mm optical path length and 2 mm<sup>2</sup> cross sectional area) when supercritical CO<sub>2</sub> was the carrier.<sup>156</sup>

The design of an NMR flow cell should provide rapid sample displacement without significant degradation of resolution. Cells similar to those in Fig. 2, with a 50  $\mu$ l observed volume work well at 1 ml/min flow-rate. The FIA injector can be connected directly to the NMR flow cell with 0.01-in i.d., 1/16-in o.d. tubing.<sup>174</sup> Sufficient premagnetization time of the sample can be accomplished by placing the injector and connectors within the magnetic field.

Special attention has been paid to interfacing FI systems and ICP.42,44-46.56.57,59.60,132,176-179 A general interface to introduce a liquid into a plasma consists of a nebulizer, a spray chamber and a separator. The main shortcomings of using conventional interfaces in FI-ICP and in LC-ICP couplings related to continuous sample aspiration are the large dead volume and the sample loss involved as well as the band broadening. Efforts have been focused on producing interfaces with high analyte transport efficiency and minimal solvent loading and dead volume in order to decrease detection limits. Low analyte transport efficiency of conventional pneumatic nebulizer/spray chamber systems (only 1-2% of the analyte aspirated actually reaches the plasma) limits the ability to analyse small sample volumes. Miniaturized interfaces have been designed<sup>42,44,45</sup> in order to overcome this drawback. The direct injection nebulizer (DIN)<sup>60</sup> is another approach to minimize the dead volume: a microconcentric nebulizer fits into the central aerosol tube of a conventional ICP torch. Solutions are nebulized directly at the base of the plasma and there is no spray chamber or separator. The microconcentric nebulizer<sup>46,59,60</sup> and thermospray nebulizer<sup>57,176,179</sup> have been the most used. In addition, miniaturized glass-frit nebulizers<sup>45</sup> have been reported to couple FIA and ICP. Solvent loading is identified as a major contributor to plasma instability and poor detection limits. A jet separator,<sup>177</sup> a condenser<sup>57,179</sup> or a membrane dryer separator<sup>132,178</sup> can be used to remove the majority of



Fig. 2. FIA-HDI interfaces. (A) NMR flow-cell and interface. (B) FIA-ICP interfaces.  $(B_1)$  Direct insertion of a microconcentric nebulizer (right) into the ICP torch (left).  $(B_2)$  Miniaturized glass-frit nebulizer.  $(B_3)$  Thermospray interface consisting of a thermospray nebulizer, a heated spray chamber and a condenser. (C) FIA-MS-MS interface. Sheet membrane probe with membrane temperature control.

the solvent and convert the sample into a dried and desolvated aerosol in a flow of argon. Membrane separators are especially useful for organic solvents.

Flow injection and mass spectrometry have been interfaced either by membrane introduction and ion spray systems. The former consists of a membrane probe directly inserted into the mass spectrometer ion source. The carrier solution flows across the inside surface of the membrane while the outside surface is exposed to the vacuum of the mass spectrometer. This interface is suitable for volatile analytes capable of diffusing through the heated membrane.<sup>163,180</sup> In ion spray MS the carrier solution is allowed to flow at a rate of 1–500  $\mu$ l/min, through a very narrow bore capillary tubing (50–200  $\mu$ m) polarized to a high voltage (2–3 kV). Spraying is facilitated by a coaxial flow of nitrogen. The electrically charged droplets found evaporate during their flight to the sampling plate (counter-electrode). The analyte must be present as an ion in solution because there is no ionization process. This injector has been connected to the ionspray interface via a 1 m × 50  $\mu$ m i.d. fused-silica tubing.<sup>162</sup>

## SAMPLE INTRODUCTION

Despite the FIA capability to carry out a series of chemical processes, the major use of flow injection-high discrimination instruments (FI-HDI) has been to transport a few  $\mu$ l of sample to the detector. In addition to this application other more interesting uses are commented on in the following sections.

An extensive use of FIA as a sample introduction tool has been done when coupled to ICP-AES<sup>41-63</sup> and ICP-MS.<sup>114-137</sup> Nevertheless, FIA–ICP hyphenated systems have profited from many other FIA capabilities.

The use of flow injection as a means of sample introduction endows the methods with a number of advantages, namely: reduced sample and reagent consumption, increased sample throughput, higher reproducibility and better detector performance.

The sample saving achievable in FI-ICP is remarkable. Sample volumes in continuous aspiration ICP are usually between 2 and 5 ml, which decreases to  $10-500 \ \mu$ l when coupled to FIA. Continuous aspiration of the sample is too wasteful to be feasible when only a limited sample volume is available (i.e. biological, clinical and forensic analysis); so the reduction of sample consumption achievable by FIA is of paramount importance in these fields. By way of example, FIA combined with ICP-AES has been successfully applied to the simultaneous determination of eight elements in 20- $\mu$ l serum samples,<sup>54</sup> and acceptable detection limits for the analysis of several metals in biological samples were obtained with the use of ca. one-hundreth of the minimum sample volume required for continuous aspiration.<sup>55</sup>

The high sample throughputs achievable by FIA are a consequence of the simple and automatic way of sample introduction, as this can be inserted into the flowing stream and monitored within few seconds, whereas standard NMR methods require at least 45-60 sec before starting monitoring.<sup>174</sup> Flow injection couplings enable near-real time monitoring thus avoiding fraction trapping, which is timeconsuming and capable of sample contamisampling with membrane nation. FI introduction MS--MS has been used for fully automated monitoring and feedback control of bioreactors.<sup>163</sup> It allows quantification of the major products and metabolites of fermentation and even detection of trace metabolites.

Flow injection is a very reproducible means to introduce a precise volume of sample and also to improve the performance of the detector by minimizing blockage drawbacks in the interface thus favouring the detector stability. The precision of transient signal integration measurements as compared to steady-state integration measurements was found to be at least one of magnitude better for all of the wear metals.52 The significant improvement in precision is due to reduced carbon build-up (more stable plasma; improved torch stability (no air pockets), constant sample solution flow-rate (use of a pump to avoid problems with viscosity changes) in the coupled FIA-ICP-AES. The ability to use small sample volumes reduces the loading of undesirable matrices on nebulizers and torches, particularly in high salt content samples or organic solvent solutions. An injection volume as low as possible without increasing detection limits must be chosen in order to minimize solid sample deposition on the torch injector tip and on the mass spectrometer sampling interface. Thus, no deposition occurs and matrix therefore reproducibility of a particular measurement is improved. This also provides better long-term stability of the instrument. The flow injection technique enables determinations in samples with total dissolved solid concentration 20-30 times higher than those handled by conventional solution aspiration. The precision of an FIA-ICP-MS approach reported by Vickers et al.<sup>114</sup> was found to be ca. twice that of a continuous flow mode, whereas Stroh et al.<sup>131</sup> have found a mean long-term stability better than 5% RSD for all the elements (10 ng/ml) they have studied in a 3% m/v NaCl matrix.

Memory effects are also minimized in an FIA-HDI coupling as the carrier immediately follows each sample plug, which results in a continuous rinsing effect that dramatically reduces clogging of the interface by deposition of

solid. The rinsing effect of the carrier decreases wash-out times, so the sampling frequency is improved as a result. Since the carrier system is flowing continuously, plasmas which normally extinguish at the air-water interface will no longer do so. In addition, injection of the sample avoids its passage through the flexible tubing of peristaltic pumps, which can adsorb the analyte<sup>116</sup> causing diminished signals and memory effects that severely degrade precision; at the same time, a close control of the flow-rate is accomplished in this way.

The use of FIA-FTIR systems provides simple and rapid sampling and easy cleaning of the flow-cell, and enables the continuous monitoring of the baseline of spectra. Pharmaceuticals<sup>154,158</sup> and pesticide formulations<sup>155</sup> have been determined successfully by FIA-FTIR thus demonstrating the usefulness of this approach.

Detection limits and spectroscopic resolution of FIA–NMR are also better than for static sample measurements.<sup>174</sup> The FI carrier solution provided a suitable medium where stable ionspray could take place in MS sample introduction.<sup>163</sup>

Solid<sup>181-184</sup> and gaseous<sup>185</sup> samples can also be introduced in FIA-HDI couplings. Despite the capability of FIA for direct introduction of solid and gaseous samples, this potential has not been exploited. Only the direct analysis of solid samples by FIA-ICP-AES has been carried out by electrolytic dissolution<sup>48</sup> and FIA-slurry atomization.63 Simultaneous determination of Zn, Si, Fe, Mn, Cr, Mg and Cu in aluminium alloys has been accomplished in a few minutes. Gaseous mixtures of compounds containing the elements Br, C, Cl and S were introduced by FIA with various sample loops (15–250  $\mu$ l) on the injection valve.<sup>46</sup> Sample gas was added to the loops at ca. 10 ml/min, then the sample carrier gas (Ar) was switched through the loops to transport their contents into the ICP.

### SAMPLE HANDLING

This section deals with some simple operations such as automatic mixing of the sample with a dilution, standard or reagent thus completing the step within a short period of time with less sample and diluent, standard or reagent consumption. An additional advantage of the automatic performance of this step is a decrease of sample manipulation and thus of the human errors arose from it. performed in an automatic way, thus achieving dilution factors for samples of standards ranging between 0 and 200. This fact justifies its coupling to HDI instead to other less versatile continuous dilution systems.<sup>70</sup> Different ways have been used to achieve this goal, namely the insertion of a short piece of wide-bore tubing, a delay coil, merging streams, zone sampling approach by using an unstirred or stirred chamber. A dilution step can be mandatory in order to minimize matrix effects in the determination of major components in a complex sample, or to fit the concentration of the analyte(s) within the linear range of determination in concentrated samples. A significant reduction of the mass-dependent interference effects without substantial sacrifice in sensitivity can be achieved by appropriate dispersion in the FI system. Vickers et al.<sup>114</sup> have demonstrated the almost complete elimination of signal suppression by using a FI manifold which provides dispersion factors up to 25. Martin and Ihrig<sup>72</sup> have developed an FI-ICP-AES approach for the automatic determination of widely varying elemental composition and concentration in a series of liquid samples without operator intervention. All the samples were appropriately diluted before determination by ICP-AES by using computer-guided sequential dilutions to place all elements within the optimum range. Sample dilution was accomplished by injecting the sample for shorter periods of time (timebased injection). The tandem-injection and merging-streams have also been employed to achieve on-line dilution and steady-state concentrations for ICP-AES and ICP-MS.<sup>64</sup>

Dilution is an FIA capability which can be

## Automatic calibration

The ability for on-line development of relatively time-consuming sample pretreatment procedures such as standard additions, internal standard, isotope dilution, and matrix-matching calibration in a simple way, saving both time and sample makes FIA a useful tool for this sample handling.

The standard-addition method has proved to be effective in overcoming matrix effects, one of the main sources of loss in both accuracy and sensitivity in certain types of samples. The FI manifold can be designed either to add the standard to the sample (before, in, or after injection) or to inject the standard into the sample (reversed FIA), among others, thus avoiding sample and standard contamination and the time-consuming preparation step.

In the reverse-FIA mode the standardaddition method is accomplished by continuous sample pumping to the detector instead of the carrier solution, the detector is zeroed for this baseline value, and the standard solutions are injected in the sample stream. The calibration curve can be run by injecting equal volumes of standards of different concentration; different volumes of the same standard solution, or using any of the FIA alternatives for dilution prior to injection. This method has been proposed to determine benzene in gasoline by FIA–FTIR,<sup>160</sup> and Si in an 85% phosphoric acid sample<sup>65</sup> and rare earth in metal samples<sup>67</sup> by FIA–ICP-AES.

Sample-standard merging before injection is an easy way to implement the standard addition method. A third stream of internal standard can merge after the sample and standard confluence.<sup>141</sup> The standard addition stream is used to add multielement standard solutions of variable concentrations. A complete standard addition can be performed in each sample by changing the standard solution. Unlike the reversed-FIA standard addition method, continuous introduction of the sample matrix into the detector is avoided by the sample standard merging method, which has been successfully used in FIA-ICP-MS<sup>142,113</sup> couplings.

The merging-zone approach has also been used for calibration purposes in the determination of Ni, Cu and Ni in alloys.<sup>68</sup> The system utilized successive injections of the sample, each one accompanied by the injection of a different standard. The limitations of this system include the relatively low sampling rate and the necessity of preparing a series of standards. The latter shortcoming might be overcome by using the zone-sampling mode, which enables controlled dilution of a given standard before its injection into the final standard carrier stream. Standard addition in plant digest samples has been implemented in an FIA-ICP-AES system by merging the sample zone with an aliquot delivered from a trapped standard zone in a modified version of the zone sampling approach. Eleven additions ranging from 3 to 32% of only one standard solution were performed in 5 min.<sup>69</sup> Nine toxic elements in undiluted urine were determined in less than 5 min using an FIA-ICP-MS approach<sup>140</sup> in which the FI manifold, which included a splitter tee, two in-parallel injection valves with different size loops (40 and 500  $\mu$ l for standard and sample, respectively) and a mixing tee, was used to inject sequentially three standard solutions into the same sample plug.

Isotope dilution was used by Lasztity, Viczian *et al.* for the determination of lead in various matrices using a merging zones approach with programmable time-based injections.

Matrix matching of sample and standards was implemented in FIA-ICP-AES by Giné *et al.*<sup>71</sup> to minimize the interferences due to easily ionizable elements. Initially the ICP determines the sodium content in the sample and thereafter the computer selects the appropriate sodium addition to match the saline concentration with that of the standards. After having received a suitable amount of sodium, the sample reaches the ICP and the elements are determined.

#### Derivatization

Flow injection is a suitable tool to carry out on-line chemical reactions in a reproducible and automatic way with a noticeable saving of both sample and reagents. The analyte can be converted into a more suitable form for detection (e.g. a volatile species which enhances the selectivity, sensitivity and scope of application of the coupled system). The chemical reactions most widely used in FIA-ICP-AES, FIA-ICP-MS FIA-MS and have been generhydride generation and vapour ation. 100-110, 148-151, 168, 169 Getek et al.<sup>167</sup> have reported an FIA-MS coupling in which electrochemical and chemical reactions took place. On-line formation and detection of glutathione and cysteine conjugates of acetaminophen were accomplished by interfacing a coulometric cell with a thermospray mass spectrometer in the flow-injection system. The electrochemical information enables the confirmation of in vivo reaction mechanisms.

#### **ON-LINE SEPARATION PROCESSES**

One of the more advantageous aspects of FIA is its availability for the development of nonchromatographic continuous separation techniques with minimal complication of the experimental set-up. Flow injection takes advantage of its dynamic nature for an easy, inexpensive implementation of separation techniques involving any of the possible interfaces (liquid-solid, liquid-liquid or gas-liquid). All of them have been implemented in on-line helped by an FI manifold, then hyphenated to a high capability instrument. The goal of the separation step has been to enhance either the sensitivity of the method by preconcentration of the target analyte(s) or the selectivity by removal of the matrix thus avoiding both its interference on the analytical signal and its passage through the detector, which is of a paramount importance in cases of insufficient or non-discrimination capability. The use of switching valves makes it feasible to lead undesirable species to the waste after separation without passing through the detection point. An additional benefit is an increased reproducibility as distortion of the signal from the analyte is minimized or avoided.

Liquid-solid interfaces have been established in FIA-HDI systems mainly by the use of solid-phase columns packed with either ion-exchange or adsorptive material, particularly with preconcentration purposes. This previous step can improve dramatically the sensitivity of a given method by one or two orders of magnitude. By way of example, the preconcentration FIA-ICP systems described by Hartenstein et al. are capable of increasing the signal by 10-15-fold and 20-75-fold per minute of sample loading time for simultaneous multielement integrated and simple element peak height, respectively, giving nearly 100% recovery of spiked analytes in tap and rain run-off waters.<sup>89</sup> Nevertheless, there are two negative aspects of these separation processes, namely: (a) The sample volume used is higher than in the absence of this step (see Tables 1-3). Depending on both the concentration of analyte in the sample and the enrichment factor to be attained the sample volume ranges between 2 and 100 ml, far from the  $\mu$ l range usual in FIA. (b) The sampling frequency decreases by a factor which depends on the working conditions. In the above example<sup>89</sup> this parameter decreased from 30-60 determinations/hr to 12-20 determinations/hr. This shortcoming can be minimized by using several columns arranged in parallel which work simultaneously and deliver sequentially the eluates to the flow manifold. The location of the column(s) in the dynamic system dramatically affects the overall performance and thus the results obtained. When the column is located in the transport zone of the flow manifold, a switching valve after the column is mandatory in order to waste undesirable sample components, thus avoiding their passage through the detector (SV<sub>2</sub> in Fig. 3A) (see Refs 81, 91, 92 and 143 as examples). The main drawback of this arrangement is the continuous



Fig. 3. Schemes of flow injection solid phase separation column coupled to high discrimination detectors. (P) Peristaltic pump; (IV) injection valve; (SV) selecting valve and (IEC) ion-exchange column.

circulation of the liquid in the same direction which tends to compact the packed material in the column and hence increases the pressure within the system. This problem can be overcome by placing the column upright and passing the solution upstream or by carrying out elution in the opposite direction of retention. The implementation of the latter approach is easy if the column is located in the loop of an injection valve (Fig. 3B). (A detailed description of the use of microcolumns in continuous flow systems can be found in Refs 12 and 13.)

In addition to the microcolumn located in any of the commented on above points, other units can be included on-line in the FI manifold to improve the efficiency of the overall process. Such is the case with the desolvation device connected to a microcolumn by Peng *et al.*<sup>91</sup> in the development of a method for the determination of trace elements by FIA–ICP-AES with on-line preconcentration. The authors achieve a desolvation efficiency of 73% at a desolvation temperature of 120°C and apply the method to



Fig. 4. Scheme of the flow injection-anodic stripping voltammetry inductively coupled plasma (FI-ASV\_ICP) approach.

the determination of Al, Cu, Cd, Fe and Mn in serum by separation of the target analytes from various co-existing elements.

A less common liquid-solid interface in FIA-HDI is that created by using an on-line voltammetric stripping cell in the flow manifold such as the arrangement depicted in Fig. 4 which has been used to deposit Cu and Cd at a working electrode, then releasing the analytes for detection by ICP-AES.<sup>147</sup> The deposition step enables the elimination of the sample matrix components that are not electroactive and do not deposit during passage of the sample through the cell, thus being sent to waste by switching the delivery valve. The target analytes were preconcentrated from sample volumes as large as necessary, then stripped for detection into a small volume of liquid of the appropriate characteristics. Detection limits of pg have been achieved for 1-ml urine samples. It must be emphasized that the sampling frequency affordable by a stripping technique is usually higher than by solid columns as both the retention and elution steps are faster. Another additional advantage of stripping is the higher efficiency of the deposition process, which can be 100%.

Liquid-liquid interfaces have seldom been established in FIA-HDI by the use of both extraction and dialysis techniques and in all of the cases the detector has been ICP-AES. In continuous liquid-liquid extraction processes the efficiency of the separation strongly depends on the aqueous-organic flow-rate ratio. One of the earlier papers in this field<sup>98</sup> reported an increase in sensitivity of ca. 250-fold in comparison with direct aspiration of an aqueous solution for the determination of Cd by ICP-AES after extraction of its diethyldithiocarbamate into carbon tetrachloride with a detection limit of 4 ng/ml and a sampling frequency of 20 hr<sup>-1</sup>. Indirect methods have also been established in this area, as is the case with the determination of fluoride in water by formation of the lanthanum/alizarin complexone/fluoride ternary complex and its extraction into hexanol containing N,N-diethylaniline. The introduction of the organic layer into the plasma and measurement of the emission intensity of La III 333.75-nm line enables the determination of the target analyte in a 0.03–1.3  $\mu$ g/ml linear range with a sampling rate of 36 samples/hr.85 Two in-series phase separators are used in order to obtain a pure organic phase to be transferred to the detector.



Fig. 5. Scheme of a flow injection- hydride generation-ICP-AES system. (P) Peristaltic pump; (IS) injection system; (CP) confluence point; (MP) mixing point; (N) nebulizer and (UT) U-tube.

A recent combination of flow injection Donnan dialysis with inductively coupled plasma atomic emission spectrometry has proved to yield enrichment factors of over 200 for cations with an 8-min dialysis time, allowing ng/ml level detection limits. These results were obtained for receiver solutions consisting either of Sr(II) or Mg(II), providing complementary free spectral ranges and the applicability of the hyphenated system to trace metal cation analysis for both transition and rare earth elements. The enrichment factors obtained were linear over a wide range of concentrations and limits of detection approximately 100 times lower than for direct aspiration. Additional improvements in enrichment factors were obtained with increases in the dialysis time and/or final sample solution temperature. A signal enhancement factor of 650 with a detection limit of 11 ng/ml for monovalent silver cation was obtained using a 30-min dialysis.<sup>94</sup> These results call for greater attention to be paid to Donnan dialysis as a powerful tool to manipulate the sensitivity of FIA-HDI methods.

Despite the small number of species capable of yielding a gas after reaction, gas-liquid interfaces have gained extensive use in FIA-HDI. Within gas-liquid separation, techniques based on hydride generation are the most common in hyphenated systems, particularly in FIA-ICP-AES and FIA-ICP-MS, where vapour generation has proved considerable enhancement of the analytical capabilities for multielemental determination of volatile vapour-forming elements at ultratrace levels in environmental samples. Very good accuracy and precision in addition to increased sensitivity and avoidance of espectral interferences caused by high salt matrix, as demonstrated in ocean

water samples.<sup>150</sup> An arrangement such as that depicted in Fig. 5 was used in one of the earlier hydride generation-FIA-ICP-AES methods. The determination of arsenic as arsine was performed at a rate of 200 injections/hr with detection limits of 1.4 ng arsenic.<sup>102</sup> Subsequent contributions have been the determination of arsenic in glycerine,<sup>103</sup> that of antimony in waste water,<sup>107</sup> and the simultaneous determination of As, Sb and Se,<sup>108</sup> among others. The simultaneous method,<sup>108</sup> as compared with continuous sample introduction, provides detection limits three times poorer. By contrast, the precision is approximately 150% better with FI due to the reduced pump pulsations. Other advantages of the FI system are the reduced sample size necessary for analysis (  $<750 \ \mu l \ vs. \ 4-5 \ ml$ for the continuous introduction system) and the potential for a greatly increased rate of sample throughput.

One of the scarce contributions on FIA–MS dealing with hydride generation is that reported by Canham and Pacey and consists of preliminary studies of the behaviour of such a system with very promising results.<sup>169</sup> A more complex FIA–ICP-MS arrangement has also been reported for the determination of hydride-generating elements and for the determination of mercury. Several pre-reduction techniques were investigated and applied to the determination of the target analytes (namely, **B**, Sb, Se, Te, Hg and As) at ultratrace levels in environmental samples. The detection limits found were in the range 0.5–7.0 pg/ml.

On-line preconcentration and oxidation by hydrogen peroxide were combined to improve the atomic emission limit of detection for iodine. The process was automated by FIA and hyphenated to both ArICP-AES and HeICP-AES for evaluation of the performance of the overall system as a way to circumvent the drawbacks encountered in the batch method, to which  $I_2$  is adsorbed onto the peristaltic PVC pump tubing causing a memory effect, and the mixed reagents were only stable for 1 hr. To minimize the memory effect in the batch method, the transfer line was rinsed with a 0.02% solution of sodium thiosulphate in an attempt to reduce I2 (adsorbed on the transfer line) to I<sup>-</sup>. Although this procedure was effective in reducing the memory effect, its use in routine analysis was limited because of cross-contamination and increased analysis time. To eliminate the cited limitations in the batch method, the reagents were mixed on-line and the formation of  $I_2$  took place along the reactor, thus avoiding its passage through the pump tubing. The iodine signal at 183.04 nm was enhanced by a factor of 33 and 100 for ArICP and HeICP, respectively, with detection limits of 5 and 9 ng/ml.<sup>82</sup>

### SPECIATION STUDIES

been implemented Speciation has in FIA-HDI using different capabilities of such arrangements. One of the simpler but more expensive ways to develop speciation is by the use of a detector which allows direct discrimination of the different forms of a given element or compound. This is the case with the FIA-MS-MS tandem, with ion-spray sample introduction and discrimination by selective reaction monitoring of daughter-parent pairs, which has been used for speciation of organotin compounds in sediment and SRM.<sup>162</sup> or the use of molecular emission cavity analysis (MECA) for the speciation of sulphur anions (as sulphide/sulphite/sulphate)<sup>172</sup> and that of phosphorus insecticides<sup>171</sup> and organophosphorus compounds, <sup>170</sup> based on the parameter  $t_{\rm M}$  ( $t_{\rm M}$ is the time elapsed between introduction of the cavity into the flame and analytical achievement of the maximum peak intensity). Speciation can also be implemented in FIA systems coupled to twin in-series detectors with non-capability for speciation. Such is the case with the speciation of phosphorus compounds (as phosphate and total phosphorus) in waste water by FIA and sequential spectrophotometry and ICP-AES. Phosphate was determined as molybdovanadophosphoric acid using a colourimetric method and the solution from the flow cell of the spectrophotometer was directly introduced to an ICP. The determination of total phosphorus was performed by measuring the emission intensity at 177.499 nm. Chromium caused a positive error in the colourimetric determination, but ions commonly existing in waste water did not interfere with the determination of total phosphorus. The sampling throughput was 80 samples/hr. The contributions of FIA to improve the features of the method were the on-line derivatization and the increased sampling frequency.<sup>112</sup>

Discrimination can also be achieved in the FI manifold. Such is the case with speciation of antimony [as Sb(III)/Sb(V)].<sup>107</sup> Antimony was reduced to stibine and determined in 1*M* malic

acid or 0.5M tartaric acid, whereas in either of these media antimony(V) gave little or no signal. Total antimony was separately determined in the presence of 0.1M thiourea as pre-reductant.

An on-line separation step can also endow the method with discriminating capability, as in the method proposed for the sequential speciation of chromium [as Cr(III)/Cr(VI)] based on the use of microcolumn of activated alumina in an FIA–ICP-AES arrangement. The column was used to separate and preconcentrate Cr(VI) from Cr(III) before ICP detection at 267.72 nm. Thus, determination limits of 1.4 and 0.20 ng/ml for Cr(III) and Cr(VI), respectively, were obtained.<sup>111</sup>

More complex separation techniques as GC have also been hyphenated to FIA and microwave-induced plasma (MIP) atomic emission spectrometry for organotin speciation analysis. The method was based on the preconcentration of ionic organotin compounds by sorption on bonded silica with octadecyl functional groups followed by on-column ethylation using sodium tetraethylborate. The derivatized species were eluted with 250  $\mu$ l of methanol, separated by gas chromatography and detected by MIP-AES. The method was applied to the determination of the target analytes in river samples which were also analysed using a manual liquid-liquid extraction method. The results agreed within 10–15% for concentrations of a few pg/ml.<sup>85</sup>

#### CONCLUSIONS

From Tables 1–3 the more extensive use of FI coupled to ICP can be stated. The first of such arrangements exploited the FI manifold only as a means of reproducible transport of the sample into the instrument, with the sole aim of increasing sample frequency. Later it was realized that periodical washing of the nebulizer is beneficial, allowing handling of concentrated samples. These features, together with the feasibility of automated dilution and calibration led to the realization that FIA is the cure of the 'Achilles heel' of ICP. From more recent developments such as FIA preconcentration/separation, FIA speciation and FIA conversion it becomes apparent that FIA can be a more useful problem solver.

The long way ran for full implementation of FIA-ICP coupling seems also to be the way followed by other high discrimination systems, as can be inferred from Tables 2 and 3. In this respect it is noticeable the scarce number of

FI-RMN methods proposed so far, despite the fact that interface problems are successfully solved as a result of the previous coupling of RMN with other hydrodynamic systems as is the case with LC-RMN.

Some isolated attempts have been made using these hyphenated systems and should be exploited as they offer interesting perspectives, namely: (a) use of robotic stations for sample pretreatment steps such as weighing and dissolution. The pretreated sample can be introduced directly into the FI manifold,<sup>186,187</sup> thus achieving full automation of the analytical process. (b) Direct introduction of solid samples into the FIA-HDI arrangement. A first attempt has been made in this respect by use of electrical energy for leaching the sample.<sup>181,182</sup> Electrolysis is not the sole way of using solid samples in these dynamic systems, as ultrasounds have also proved their great potential in this context.<sup>183,184</sup> (c) Use of FIA as a 'hyphen' allowing different instrumental techniques to be linked together. The use of a stripping flow-cell for preconcentration purposes is a partial example of this potential, which can also be expanded to its use for preconcentration/determination prior to the high discrimination instrument, thus increasing the information level. Also FIA could be linked to apparatus such as a supercritical fluid extractor and an HDI with accomplishment of the intermediate step (derivatization, separation, etc.), which no doubt would improve the overall performance of the method. (d) The scope of non-chromatographic continuous separation techniques coupled to FIA-HDI should be broadened by including prevaporation<sup>188</sup> and continuous precipitation<sup>189</sup> as both have proved their capabilities when coupled to FIA. (e) More attention must be paid to the use of FIA to obtain information in the development of theoretical studies of the dynamics in membrane and membraneless instruments,<sup>180</sup> and to the FIA-HDI coupling interfaced by an autosampler.<sup>190</sup> All these slightly or unexploited aspects of FIA in hyphenated systems can undergo suitable development with the present trend of some manufacturers, which integrate FIA systems in HDI as a means, in principle, of sample handling.

Acknowledgement—Comisión Interministerial de Ciencia y Tecnología (CICyT) is thanked for financial support.

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